

A circular inclusion with inhomogeneous sliding imperfect interface in harmonic materials

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Abstract. In the following study we rigorously analyze the problem of a circular inclusion with inhomogeneous imperfect sliding interface in finite deformation of harmonic materials. The work begins by defining the inhomogeneous sliding boundary conditions characterized by two imperfect interface parameters $m(\theta) \rightarrow \infty$ and $n(\theta) = \textit{finite}$ corresponding to the normal and tangential coordinate directions (with respect to the interface boundary curve), respectively. Then, through the process of analytic continuation the problem is eventually reduced to the determination of a single analytic function given by an ordinary differential equation with variable coefficients. A specific example is selected to illustrate the method. The effects of the circumferential variation of the interface parameter on the mean stress at the interface and the average mean stress in the inclusion are discussed.

Keywords. Inclusion, Harmonic material, Imperfect interface.

1. Introduction

The study of inclusion problems in the linear theory of elasticity has seen a great deal of development over the past decades. The research conducted in this area ranges from the fundamental works of Eshelby [1] and Muskhelishvili [2], amongst others, which utilized perfect bonding conditions and ellipsoidal geometries, to the introduction of arbitrary inclusion geometries (see, for example [3, 4, 5]), imperfect bonding models (see, for example [6, 7, 8]) and complex interphase models (see, for example [9]) in more recent years. On the contrary, inclusion problems in finite elasticity theory, specifically in the area of harmonic materials, has not seen the same degree of interest or success. The works of Fritz [10], Ogden and Isherwood [11], Varley and Cumberbatch [12], Knowles and Sternberg [13] laid the foundation for the finite deformation of harmonic materials. However, it was not until Ru [14] who developed a more convenient form of the complex variable formulation for harmonic materials that research into inclusion problems experienced rapid growth. Building on this work, finite elasticity problems of elliptical inclusions with uniform internal stress fields [15], designing an inclusion with uniform interior stress [16], partially debonded circular inclusions [17] and a circular inclusion with homogeneous imperfect interface [18] have been studied just to name a few. However, in many real world problems a homogeneous imperfect interface is not a realistic assumption. Hence, what is of particular interest is a model that captures the variability of interface damage (such as the presence of microcracks, voids and impurities) which is referred to as an inhomogeneous imperfect interface. This assertion is supported, in part, by previous works (see [19, 20]) corresponding to an inhomogeneous spring-type interface and an inhomogeneous non-slipping interface, respectively.

Recently, the concept of a sliding boundary has been receiving increasing interest in the literature since the study of sliding boundaries is necessary for modelling critical features of material behaviour. In 1993 Mijailovich et al. ([21]) hypothesized that dissipative stresses arise in the interaction among

fibers in connective lung tissue matrix. They established a mechanistic model by reducing the complicated three dimensional fiber network to the interaction of two ideal fibers that dissipate energy along their common slipping interface surface. The resulting model illustrates that a slipping interface is critical in understanding the mechanisms behind connective tissue elasticity. In the area of material science, it has been demonstrated through atomistic simulations (see, for example, Van Swygenhoven ([22]) that for nanocrystalline materials macroscopic imposed deformations are accommodated by grain boundary slipping and separation. Following this fact Wei et al. ([23]) considered the effects of grain boundaries on polycrystalline materials. By incorporating crystal plasticity for the grain interior together with an interface constitutive model that takes into account grain boundary related deformation at the interface the authors illustrate that grain boundary slip-separation deformation has a significant effect on material response. Barton et al. ([24]) developed a multi-material numerical scheme for non-linear elastic solids that examines interfacial boundary conditions with particular emphasis placed on a sliding interface. Several examples are provided to illustrate the scheme.

In this work we consider the inhomogeneous sliding imperfect interface (where the interphase layer is modeled as a 2-dimensional curve of vanishing thickness and the material properties of the interphase layer are given as spring-type interface parameters) where the interfacial bonding is characterized by $m(\theta) \rightarrow \infty$ and $n(\theta) = \text{finite}$ (where $m(\theta)$ and $n(\theta)$ are the normal and tangential imperfect interface parameters, respectively describing the variability of interphase damage and θ is the polar angle). Such an interface condition allows for a relative tangential displacement but maintains continuity of radial displacements across the interphase layer. Use of the inhomogeneous sliding imperfect interface for the case of finite deformation is suitable for applications where type 1 harmonic materials are considered as it was demonstrated by Varley et al [12] that for type 1 harmonic materials the differences in the principal Piola stresses are linearly proportional to the difference in the stretch ratios.

The work begins with section 2 where the fundamental equations of type 1 harmonic materials are presented. Following section 2, section 3 discusses the formulation of the problem and the sliding boundary conditions where eventually a first order linear ordinary differential equation with variable coefficients is developed for the inclusion function. Section 4 illustrates the analysis for a specific class of imperfect interface and in section 5 an example is given to illustrate the method. In section 6 the average mean stress in the inclusion and the mean stress at a point on the interface is evaluated and compared to the corresponding homogeneous imperfect interface. Finally a summary of the results are presented in section 7.

2. Mathematical Preliminaries

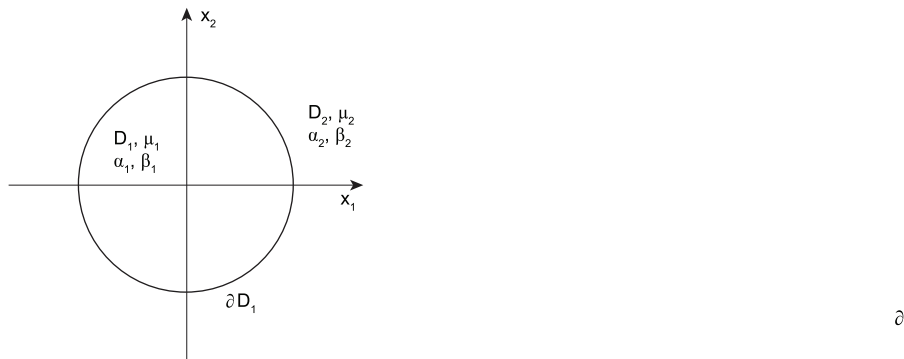


FIGURE 1. Elastic circular inclusion(D_1) bounded by curve ∂D_1 embedded in a infinite matrix (D_2)

Consider a single simply connected domain bounded by a continuous circular curve ∂D_1 , embedded in an infinite matrix in \mathbb{R}^2 . Let us assume that any deformation relative to the reference configuration is

confined to the x_1x_2 plane. Let $z = x_1 + ix_2$ be the Lagrangian coordinates of a particle in the reference configuration and let $w(z) = y_1(z) + iy_2(z)$ be the Eulerian coordinates of a particle in the current configuration. The inclusion is denoted by D_1 and endowed with material properties μ_1, α_1, β_1 . The matrix is denoted by domain D_2 with material properties μ_2, α_2, β_2 where $\frac{1}{2} \leq \alpha_k < 1, \beta_k > 0, k = 1, 2$. In both cases, μ represents the material shear modulus, and α, β are derived from the ratios of the principal stretches of a harmonic material under uni-axial tension. The matrix and inclusion are assumed to be type 1 harmonic materials with a strain energy function $W(I, J)$ defined as follows

$$(2.1) \quad W(I, J) = 2\mu [H(R) - J], \quad F_{ij} = \frac{\partial y_i}{\partial x_j}, \quad H'(R) = \frac{1}{4\alpha} \left[R + \sqrt{R^2 - 16\alpha\beta} \right],$$

where I and J are the scalar invariants of the right Cauchy Green tensor $\mathbf{F}^T \mathbf{F}$ corresponding to the two dimensional deformation as noted above and are given by

$$(2.2) \quad I = \lambda_1^2 + \lambda_2^2 = \text{tr}[\mathbf{C}], \quad J = \lambda_1 \lambda_2 = \sqrt{\det[\mathbf{C}]} = \det[\mathbf{F}],$$

where λ_1, λ_2 are the principal stretches and $R = \sqrt{I + 2J}$. According to Ru [14], the deformation map and the Piola stress function can be given in terms of two complex potential functions $\phi_k(z)$ and $\psi_k(z)$ as follows

$$(2.3) \quad \begin{aligned} iw_k(z, \bar{z}) &= \alpha_k \phi_k(z) + i\overline{\psi_k(z)} + \frac{\beta_k z}{\phi'_k(z)}, \\ \chi_k(z, \bar{z}) &= 2i\mu_k \left[(\alpha_k - 1)\phi_k(z) + i\overline{\psi_k(z)} + \frac{\beta_k z}{\phi'_k(z)} \right], \quad \text{for } k = 1, 2. \end{aligned}$$

Equation (2.3) gives rise to the following Cartesian expressions for the stress and displacement fields

$$(2.4) \quad \begin{aligned} w_k(z, \bar{z}) - z &= (u_1 + iu_2)_k, \\ \chi_k(z, \bar{z})_{,1} &= (P_{22} - iP_{12})_k, \quad \chi_k(z, \bar{z})_{,2} = (-P_{21} + iP_{11})_k, \quad k = 1, 2. \end{aligned}$$

where the subscript k refers to either the inclusion $k = 1$ or the matrix $k = 2$.

In order to illustrate the significance of the inhomogeneous sliding imperfect interface we consider the scenario where the rotations are neglected. Then equation (2.4) may be transformed into polar coordinates as shown:

$$(2.5) \quad \frac{R}{z} w_k(z, \bar{z}) - R = (u_r + iu_\theta)_k, \quad \chi'_k(z, \bar{z}) = (P_{rr} + iP_{\theta r})_k, \quad k = 1, 2.$$

where a prime (') denotes differentiation with respect to z .

3. Formulation

Assuming that the inclusion is imperfectly bonded to the matrix along ∂D_1 the general imperfect interface conditions are given by

$$(3.1) \quad \|P_{rr} + iP_{\theta r}\| = 0, \quad P_{rr} = m(\theta) \|u_r\|, \quad P_{\theta r} = n(\theta) \|u_\theta\|, \quad z \in \partial D_1,$$

where $m(\theta)$ and $n(\theta)$ are two non-negative imperfect interface parameters and $\|.\| = (.)_2 - (.)_1$ is the quantitative jump across ∂D_1 . It is assumed that the potential functions $\phi_2(z)$ and $\psi_2(z)$ exhibit the following asymptotic behavior as $|z| \rightarrow \infty$

$$(3.2) \quad \phi_2(z) = Az + O(1), \quad \psi_2(z) = Bz + O(1), \quad |z| \rightarrow \infty,$$

where A and B are complex constants that reflect the far-field loading and are given by [19]

$$(3.3) \quad A = i \left[\frac{\frac{P_{22}^\infty + P_{11}^\infty}{4\mu_2} \pm \sqrt{\left(\frac{P_{22}^\infty + P_{11}^\infty}{4\mu_2}\right)^2 + 4(1 - \alpha_2)\beta_2}}{2(1 - \alpha_2)} \right],$$

$$(3.4) \quad B = \frac{P_{11}^\infty - P_{22}^\infty - 2iP_{12}^\infty}{4\mu_2},$$

and the $O(1)$ are some first order constant terms. Furthermore, since ϕ_k, ψ_k are potential functions, we only consider the case where they are analytic and hence the potentials $\phi_k(z)$ and $\psi_k(z)$, $k = 1, 2$ admit the following series expansions

$$(3.5) \quad \begin{aligned} \phi_1(z) &= X_0 + \sum_{k=1}^{\infty} X_k z^k, \quad \psi_1(z) = Y_0 + \sum_{k=1}^{\infty} Y_k z^k, \quad z \in D_1, \\ \phi_2(z) &= Az + \sum_{k=0}^{\infty} A_k z^{-k}, \quad \psi_2(z) = Bz + \sum_{k=0}^{\infty} B_k z^{-k}, \quad z \in D_2. \end{aligned}$$

Remark 1. From (3.5) we require that $X_1 \neq 0$ for $|z| \leq R$ and $A \neq 0$ for $|z| \geq R$. This guarantees that $F'(I) = |\phi'_k(z)| \neq 0 \quad \forall z \in \mathbb{C}$.

In the present work we do not consider a rigid displacement of the inclusion, hence, without loss of generality, it is admissible to set both $X_0, Y_0 = 0$ and the continuity of traction condition from (3.1) gives

$$(3.6) \quad \mu_1 \left[(\alpha_1 - 1) \phi_1(z) + i\overline{\psi_1}(R^2/z) + \frac{\beta_1 z}{\phi_1'(R^2/z)} \right] = \\ \mu_2 \left[(\alpha_2 - 1) \phi_2(z) + i\overline{\psi_2}(R^2/z) + \frac{\beta_2 z}{\phi_2'(R^2/z)} \right], \quad z \in \partial D_1.$$

Substituting $\Gamma = \frac{\mu_1}{\mu_2}$ into the above yields

$$(3.7) \quad \Gamma(\alpha_1 - 1)\phi_1(z) - i\overline{\psi_2}(R^2/z) - \frac{\beta_2 z}{\phi_2'(R^2/z)} = \\ (\alpha_2 - 1)\phi_2(z) - \Gamma i\overline{\psi_1}(R^2/z) - \frac{\Gamma\beta_1 z}{\phi_1'(R^2/z)}, \quad z \in \partial D_1.$$

The LHS of (3.7) is analytic for $z \in D_1$ and the RHS is analytic for $z \in D_2$. Utilizing the principle of analytic continuation on (3.7) we arrive at the following

$$(3.8) \quad i\overline{\psi_2}(R^2/z) + \frac{\beta_2 z}{\phi_2'(R^2/z)} = \Gamma(\alpha_1 - 1)\phi_1(z) - (\alpha_2 - 1)Az + \frac{\Gamma\beta_1 z}{X_1} + \frac{i\overline{B}R^2}{z}, \quad z \in \partial D_1,$$

and

$$(3.9) \quad i\overline{\psi_1}(R^2/z) + \frac{\beta_1 z}{\phi_1'(R^2/z)} = \frac{(\alpha_2 - 1)}{\Gamma}\phi_2(z) - \frac{(\alpha_2 - 1)}{\Gamma}Az + \frac{\beta_1 z}{X_1} + \frac{i\overline{B}R^2}{\Gamma z}, \quad z \in \partial D_1.$$

Thus, the problem is now reduced to determining two unknown analytic functions $\phi_1(z)$ and $\phi_2(z)$ complying with the interface condition and the asymptotic condition for $\phi_2(z)$.

3.1. Solution for Homogeneous Imperfect Interface

In this section we will briefly examine the homogeneous imperfect interface where the parameters m and n appearing in (3.29) are assumed to be constant along ∂D_1 . Although a similar problem has been investigated by Wang[18], for ease of comparison, we present a solution that is more amenable to validating the present work.

The general form of the imperfect interface condition is given as

$$(3.10) \quad (P_{rr} + iP_{\theta r})_2 = \frac{m+n}{2} \|u_r + iu_\theta\| + \frac{m-n}{2} \|u_r - iu_\theta\|, \quad z \in \partial D_1,$$

Inserting the definitions of (2.5) into (3.10) yields

$$(3.11) \quad i\chi_2'(z) = \frac{(m+n)R}{2z} (iw_2(z) - iw_1(z)) + \frac{(m-n)z}{2R} (\overline{iw_1}(R^2/z) - \overline{iw_2}(R^2/z)), \quad z \in \partial D_1.$$

Next, substituting in (3.8,3.9) into (3.11) gives

$$(3.12) \quad \begin{aligned} (1 - \alpha_2)\phi_2'(z) + \Gamma(1 - \alpha_1)\phi_1'(z) + (\alpha_2 - 1)A - \frac{\Gamma\beta_1}{\overline{X}_1} + \frac{i\overline{B}R^2}{z^2} &= \frac{(m+n)R}{4\mu_2} \left[\frac{\phi_2(z)}{z} \left(\frac{\alpha_2\Gamma - \alpha_2 + 1}{\Gamma} \right) \right. \\ &+ \frac{\phi_1(z)}{z} (\Gamma(\alpha_1 - 1) - \alpha_1) + A \left(\frac{\alpha_2 - 1}{\Gamma} - \alpha_2 + 1 \right) + \frac{\beta_1(\Gamma - 1)}{\overline{X}_1} + \frac{i\overline{B}R^2}{z^2} \frac{\Gamma - 1}{\Gamma} \Big] + \\ &\frac{m-n}{4\mu_2 R} \left[z\overline{\phi_1}(R^2/z)(\alpha_1 - \Gamma(\alpha_1 - 1)) + z\overline{\phi_2}(R^2/z) \left(\frac{\alpha_2 - 1}{\Gamma} - \alpha_2 \right) + \overline{A}R^2(\alpha_2 - 1 - \frac{\alpha_2 - 1}{\Gamma}) \right. \\ &\left. + \frac{\beta_1 R^2(1 - \Gamma)}{X_1} + iBz^2 \frac{(\Gamma - 1)}{\Gamma} \right], \quad z \in \partial D_1. \end{aligned}$$

Substituting the definitions of (3.5) into (3.12) and performing analytic continuation yields the following expression as a compatibility condition between the two resulting functions

$$(3.13) \quad \Gamma(1 - \alpha_1)X_1 - \frac{\Gamma\beta_1}{\overline{X}_1} = \frac{mR}{4\mu_2} \left[(\Gamma(\alpha_1 - 1) - \alpha_1)(X_1 - \overline{X}_1) + \beta_1(\Gamma - 1) \left(\frac{1}{\overline{X}_1} - \frac{1}{X_1} \right) + 2A \right] \\ + \frac{nR}{4\mu_2} \left[(\Gamma(\alpha_1 - 1) - \alpha_1)(X_1 + \overline{X}_1) + \beta_1(\Gamma - 1) \left(\frac{1}{\overline{X}_1} + \frac{1}{X_1} \right) \right],$$

As an example, it can be shown that (3.13) may be rearranged into

$$(3.14) \quad \left[\frac{R(m+n)}{4\mu_1} + \frac{1 - \alpha_1}{\alpha_1 + \Gamma(1 - \alpha_1)} \right] X_1 + \frac{(n-m)R}{4\mu_1} \overline{X}_1 + \\ \frac{\beta_1}{\alpha_1 + \Gamma(1 - \alpha_1)} \left[\frac{\frac{(m+n)R}{4\mu_1}(1 - \Gamma) - 1}{\overline{X}_1} + \frac{\frac{(n-m)R}{4\mu_1}(1 - \Gamma)}{X_1} \right] = \frac{\frac{ARm}{2\mu_1}}{\alpha_1 + \Gamma(1 - \alpha_1)},$$

which is identical to the results provided by Wang, save for the insertion that A is purely imaginary, in [18].

Noting that as either $(m$ or $n) \rightarrow \infty$ in (3.13) we recover only the displacement continuity boundary condition, we must further evaluate the stress-displacement condition given by

$$(3.15) \quad \frac{(P_{rr})_2}{m} + i \frac{(P_{r\theta})_2}{n} = \|u_r + iu_\theta\|, \quad z \in \partial D_1,$$

which degenerates to

$$(3.16) \quad \frac{\chi_2'(z) - \overline{\chi_2'}(R^2/z)}{2i} = -in \frac{R}{z} [w_2(z) - w_1(z)], \quad z \in \partial D_1,$$

as $m \rightarrow \infty$. Substituting the definitions of $\chi_2(z)$ and $w_k(z)$, $k = 1, 2$ into (3.16) and comparing coefficients of like powers of z on the LHS and RHS gives the following

$$(3.17) \quad \Gamma(\alpha_1 - 1)(X_1 + \overline{X_1}) + \Gamma\beta_1 \left(\frac{1}{X_1} + \frac{1}{\overline{X_1}} \right) = \frac{nR}{\mu_2} \left[(\alpha_1 - \Gamma(\alpha_1 - 1))X_1 + (1 - \Gamma)\frac{\beta_1}{\overline{X_1}} - A \right], (z^0),$$

$$(3.18) \quad X_2 = A_0 = 0, (z^{\pm 1}),$$

$$(3.19) \quad 3\Gamma(\alpha_1 - 1)X_3 + (1 - \alpha_2)\frac{\overline{A_1}}{R^4} + \frac{iB}{R^2} = \frac{nR}{\mu_2} [(\alpha_1 - \Gamma(\alpha_1 - 1))X_3], (z^2),$$

$$(3.20) \quad (1 - \alpha_2)A_1 + 3\Gamma(\alpha_1 - 1)\overline{X_3}R^4 - i\overline{B}R^2 = \frac{nR}{\mu_2} \left[i\overline{B}R^2 \frac{(1 - \Gamma)}{\Gamma} + \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} A_1 \right], (z^{-2}),$$

$$(3.21) \quad A_k = X_{k+2} = 0, \forall k \geq 2.$$

If we then input the compatibility condition from (3.13) into (3.17) for the case of $m \rightarrow \infty$ we arrive at the following expression for X_1 and $\overline{X_1}$

$$(3.22) \quad \Gamma(1 - \alpha_1)(\overline{X_1} + X_1) - \Gamma\beta_1 \left(\frac{1}{X_1} + \frac{1}{\overline{X_1}} \right) = \frac{nR}{\mu_2} [(\Gamma(\alpha_1 - 1) - \alpha_1)(X_1 + \overline{X_1}) + (\Gamma - 1)\beta_1 \left(\frac{1}{\overline{X_1}} + \frac{1}{X_1} \right)].$$

Equation (3.22) implies that $Re[X_1] = 0$ and that X_1 being purely imaginary is given by

$$(3.23) \quad (\alpha_1 - \Gamma(\alpha_1 - 1))X_1 + (1 - \Gamma)\frac{\beta_1}{\overline{X_1}} - A = 0.$$

3.2. Inhomogeneous Imperfect Sliding Interface

We shall now consider a circular inclusion for which the inhomogeneous imperfect interface is characterized by $m(\theta) \rightarrow \infty$, $n(\theta) = finite$. For this so called sliding interface the boundary conditions take the form

$$(3.24) \quad \frac{(P_{r\theta})_2}{n(\theta)} = ||u_\theta||, \quad ||u_r|| = 0, \quad z \in \partial D_1,$$

where $n(\theta)$ is non-negative and periodic along ∂D_1 . The displacement continuity condition is evaluated as follows

$$(3.25) \quad ||u_r|| = \frac{R}{z} (iw_2(z) - iw_1(z)) + \frac{z}{R} (\overline{iw_1}(R^2/z) - \overline{iw_2}(R^2/z)), \quad z \in \partial D_1.$$

Inserting (2.3) in combination with (3.8,3.9) into (3.25) gives

$$\begin{aligned}
 (3.26) \quad & [\Gamma(\alpha_1 - 1) - \alpha_1] \frac{R}{z} \phi_1(z) + \left[\frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \right] \frac{z}{R} \overline{\phi_2}(R^2/z) + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} AR \\
 & + \frac{iBz^2}{R} \frac{\Gamma - 1}{\Gamma} + \frac{\beta_1}{X_1} (1 - \Gamma) = [\Gamma(\alpha_1 - 1) - \alpha_1] \frac{z}{R} \overline{\phi_1}(R^2/z) + \left[\frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \right] \frac{R}{z} \phi_2(z) \\
 & + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{AR} + \frac{i\overline{B}R^3}{z^2} \frac{1 - \Gamma}{\Gamma} + \frac{\beta_1}{X_1} (1 - \Gamma), \quad z \in \partial D_1.
 \end{aligned}$$

In (3.26) the left hand side is analytic in D_1 and the right hand side is analytic in D_2 except for possibly at the point $|z| = 0$ and as $|z| \rightarrow \infty$, respectively. Employing the technique of analytic continuation, we first analyze the behavior of the left hand side of (3.26) as $|z| \rightarrow 0$ as follows

$$(3.27) \quad (\Gamma(\alpha_1 - 1) - \alpha_1) X_1 R + \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \overline{AR} + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} AR + \frac{\beta_1}{X_1} (1 - \Gamma), \quad |z| \rightarrow 0.$$

Since (3.27) does not contain any strictly singular terms, we may conclude that the left hand side of (3.26) is analytic in D_1 as $|z| \rightarrow 0$. Moving on to the right hand side of (3.26), we observe the following as $|z| \rightarrow \infty$

$$(3.28) \quad (\Gamma(\alpha_1 - 1) - \alpha_1) \overline{X_1} R + \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} AR + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{AR} + \frac{\beta_1}{X_1} (1 - \Gamma), \quad |z| \rightarrow \infty.$$

Equation (3.28) represents the asymptotic behavior of the right hand side of (3.26) and, subtracting (3.28) from both sides of (3.26), we may form the following function

$$(3.29) \quad D(z) = \begin{cases} [\Gamma(\alpha_1 - 1) - \alpha_1] \frac{R}{z} \phi_1(z) + \left[\frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \right] \frac{z}{R} \overline{\phi_2}(R^2/z) + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} AR \\ + \frac{iBz^2}{R} \frac{\Gamma - 1}{\Gamma} + \frac{\beta_1}{X_1} (1 - \Gamma) - (\Gamma(\alpha_1 - 1) - \alpha_1) \overline{X_1} R - \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} AR - \\ \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{AR} - \frac{\beta_1}{X_1} (1 - \Gamma), \quad z \in D_1 \\ \\ [\Gamma(\alpha_1 - 1) - \alpha_1] \frac{z}{R} \overline{\phi_1}(R^2/z) + \left[\frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \right] \frac{R}{z} \phi_2(z) \\ + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{AR} + \frac{i\overline{B}R^3}{z^2} \frac{1 - \Gamma}{\Gamma} + \frac{\beta_1}{X_1} (1 - \Gamma) - \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} AR - \\ \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{AR} - \frac{\beta_1}{X_1} (1 - \Gamma), \quad z \in D_2. \end{cases}$$

Now, since $D(z)$ is well defined and analytic in the entire plane including as $|z| \rightarrow \infty$, Louisvilles theorem states that $D(z) = \text{constant}$. This implies, through the subtraction of (3.28) on the left hand and right hand side of (3.26), that $D(z) = 0$ and hence we arrive at the following two equations

$$\begin{aligned}
 (3.30) \quad & [\Gamma(\alpha_1 - 1) - \alpha_1] \frac{R}{z} \phi_1(z) + \left[\frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \right] \frac{z}{R} \overline{\phi_2}(R^2/z) + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} AR \\
 & + \frac{iBz^2}{R} \frac{\Gamma - 1}{\Gamma} + \frac{\beta_1}{X_1} (1 - \Gamma) - (\Gamma(\alpha_1 - 1) - \alpha_1) \overline{X_1} R - \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} AR - \\
 & \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{AR} - \frac{\beta_1}{X_1} (1 - \Gamma) = 0, \quad z \in D_1,
 \end{aligned}$$

$$\begin{aligned}
(3.31) \quad & [\Gamma(\alpha_1 - 1) - \alpha_1] \frac{z}{R} \overline{\phi_1}(R^2/z) + \left[\frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \right] \frac{R}{z} \phi_2(z) \\
& + \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{A}R + \frac{i\overline{B}R^3}{z^2} \frac{1 - \Gamma}{\Gamma} + \frac{\beta_1}{\overline{X_1}}(1 - \Gamma) - \frac{\alpha_2 - 1 - \Gamma\alpha_2}{\Gamma} \overline{A}R - \\
& \frac{\alpha_2 - 1 + \Gamma(1 - \alpha_2)}{\Gamma} \overline{A}R - \frac{\beta_1}{\overline{X_1}}(1 - \Gamma) = 0, \quad z \in D_2.
\end{aligned}$$

The compatability requirement between equations (3.30) and (3.31) is given by

$$(3.32) \quad (\Gamma(\alpha_1 - 1) - \alpha_1)(X_1 - \overline{X_1}) + \beta_1(1 - \Gamma) \left(\frac{1}{X_1} - \frac{1}{\overline{X_1}} \right) = -2A.$$

We now consider the tangential stress-displacement interface condition which may be written as

$$(3.33) \quad \frac{(P_{r\theta})_2}{n(\theta)} = -i||u_r + iu_\theta||, \quad z \in \partial D_1,$$

which, in terms of (2.3,2.4) and (3.8,3.9,3.31,3.33) becomes

$$\begin{aligned}
(3.34) \quad & \left[\frac{\Gamma(1 - \alpha_2 + \Gamma(1 - \alpha_1))}{\alpha_2 - 1 - \Gamma\alpha_2} \right] \phi_1'(z) + \left[\frac{\Gamma(1 - \alpha_2 + \Gamma(1 - \alpha_1))}{\alpha_2 - 1 - \Gamma\alpha_2} \right] \overline{\phi_1}'(R^2/z) + \\
& \frac{2\Gamma(\alpha_2 - 1)(\alpha_1 - \Gamma(\alpha_1 - 1))}{\alpha_2 - 1 - \Gamma\alpha_2} \frac{\phi_1(z)}{z} + \frac{2\Gamma(\alpha_2 - 1)(\alpha_1 - \Gamma(\alpha_1 - 1))}{\alpha_2 - 1 - \Gamma\alpha_2} \overline{\phi_1}'(R^2/z) \frac{z}{R^2} \\
& + \frac{i\overline{B}R^2}{z^2} \frac{\Gamma}{\alpha_2 - 1 - \Gamma\alpha_2} - \frac{iBz^2}{R^2} \frac{\Gamma}{\alpha_2 - 1 - \Gamma\alpha_2} + \frac{\Gamma(\alpha_2 - 1)(\Gamma(\alpha_1 - 1) - \alpha_1)}{\alpha_2 - 1 - \Gamma\alpha_2} \frac{1}{\overline{X_1}} \\
& + \frac{\Gamma(\alpha_2 - 1)(\Gamma(\alpha_1 - 1) - \alpha_1)}{\alpha_2 - 1 - \Gamma\alpha_2} X_1 + \frac{\Gamma\beta_1}{\overline{X_1}} + \frac{\Gamma\beta_1}{X_1} = \\
& \frac{n(\theta)R}{\mu_2} \left[(\alpha_1 - \Gamma(\alpha_1 - 1)) \frac{\phi_1(z)}{z} + (\alpha_1 - \Gamma(\alpha_1 - 1)) \frac{z}{R^2} \overline{\phi_1}(R^2/z) + \right. \\
& \left. (\Gamma(\alpha_1 - 1) - \alpha_1) \frac{\overline{X_1}}{2} + \frac{\beta_1}{2\overline{X_1}}(1 - \Gamma) + (\Gamma(\alpha_1 - 1) - \alpha_1) \frac{X_1}{2} + \frac{\beta_1}{2X_1}(1 - \Gamma) \right], \quad z \in \partial D_1.
\end{aligned}$$

The problem is now reduced to determining the single analytic function $\phi_1(z)$. Unlike the homogeneous analog, direct substitution of the power series expansion of $\phi_1(z)$ into (3.34) will result in an unsolvable system of equations for the coefficients of $\phi_1(z)$. As such, we shall seek to use analytic continuation to further reduce (3.34) into an ordinary differential equation with variable coefficients for $\phi_1(z)$. To aid in this process we will define a new imperfect interface parameter to replace $n(\theta)$ in (3.34) as follows

$$(3.35) \quad \delta(\theta) = \frac{n(\theta)R}{\mu_2}, \quad \delta(\theta) > 0,$$

and since $1/\delta(\theta)$ is a non-negative and periodic function on ∂D_1 , we may write

$$(3.36) \quad \frac{\delta_0}{\delta(\theta)} = 1 + f(\theta), \quad \delta_0 > 0, \quad f(\theta) > -1,$$

where δ_0 is real, $f(\theta)$ is 2π periodic on ∂D_1 , and as $f(\theta) \rightarrow -1$, $n(\theta) \rightarrow \infty$, which is the case of a perfectly bonded interface. Given $f(\theta)$ is 2π periodic on ∂D_1 we are afforded a Fourier series expansion for $(1 + f(z))$ which we may then rewrite as a function of the complex variable z as follows

$$(3.37) \quad f(z) = \frac{1}{2} \sum_{k=1}^s (b_k + ia_k) \frac{R^k}{z^k} + (b_k - ia_k) \frac{z^k}{R^k}, \quad \forall z \in \partial D_1, f(\theta) = f(z).$$

3.3. The Differential Equation for $\phi_1(z)$

Before returning to (3.34) we introduce the following two material parameters

$$(3.38) \quad \Omega = \frac{(1 - \alpha_2)(\alpha_1 - \Gamma(\alpha_1 - 1))}{1 - \alpha_2 + \Gamma(1 - \alpha_1)} > 0, \quad \omega = \frac{\Gamma\alpha_2 - \alpha_2 + 1}{1 - \alpha_2 + \Gamma(1 - \alpha_1)} > 0.$$

Using (3.36,3.37,3.38) we may rewrite (3.34) as

$$(3.39) \quad (1 + f(z))\phi_1'(z) + \left[\frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{z} - \frac{2\Omega(1 + f(z))}{z} \right] \phi_1(z) + \\ (1 + f(z)) \left[\Omega X_1 - \frac{iBz^2}{R^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} - \frac{\omega\beta_1}{X_1} \right] - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{2} X_1 + \\ \frac{\beta_1}{2X_1} \frac{(1 - \Gamma)\omega\delta_0}{\Gamma} = -(1 + f(z))\overline{\phi_1'}(R^2/z) + \\ \left[\frac{2\Omega(1 + f(z))z}{R^2} - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{R^2} \right] \overline{\phi_1}(R^2/z) - \\ (1 + f(z)) \left[\Omega \overline{X_1} - \frac{\omega\beta_1}{\overline{X_1}} + \frac{i\overline{B}R^2}{z^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \right] + \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{2} \overline{X_1} - \\ \frac{\beta_1}{2\overline{X_1}} \frac{(1 - \Gamma)\delta_0\omega}{\Gamma}, \quad z \in \partial D_1.$$

The left hand side of (3.39) is analytic in D_1 and the right hand side is analytic in D_2 . Using the technique of analytic continuation we may construct an entire function by studying the behaviour of the left hand and right hand side of (3.39) as $|z| \rightarrow 0$, and $|z| \rightarrow \infty$, respectively. Beginning with the left hand side we allow $|z| \rightarrow 0$ and recover the following singular terms

$$(3.40) \quad \sum_{j=1}^k j X_j z^{j-1} \sum_{k=1}^s \frac{b_k + ia_k}{2} \frac{R^k}{z^k} - 2\Omega \sum_{j=1}^k X_j z^{j-1} \sum_{k=1}^s \frac{b_k + ia_k}{2} \frac{R^k}{z^k} + \\ \left[\Omega X_1 - \frac{\omega\beta_1}{X_1} \right] \sum_{k=1}^s \frac{b_k + ia_k}{2} \frac{R^k}{z^k} - \frac{iB\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \sum_{k=3}^s \frac{b_k + ia_k}{2} \frac{R^{k-2}}{z^{k-2}}, \quad |z| \rightarrow 0.$$

Proceeding to the right hand side of (3.39), we find the following asymptotic and singular behavior as $|z| \rightarrow \infty$

$$\begin{aligned}
(3.41) \quad & \overline{X_1}(\Omega - 1) - \sum_{k=1}^k j \overline{X_j} \left(\frac{R^2}{z} \right)^{j-1} \sum_{k=1}^s \frac{b_k - ia_k}{2} \frac{z^k}{R^k} - \sum_{k=1}^s (k+1) \overline{X_{k+1}} \frac{b_k - ia_k}{2} R^k + \\
& 2\Omega \left[\sum_{j=1}^k \overline{X_j} \left(\frac{R^2}{z} \right)^{j-1} \sum_{k=1}^s \frac{b_k - ia_k}{2} \frac{z^k}{R^k} + \sum_{k=1}^s \overline{X_{k+1}} \frac{b_k - ia_k}{2} R^k \right] - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0}{2} \overline{X_1} + \\
& \frac{\omega\beta_1}{\overline{X_1}} - \left[\Omega \overline{X_1} - \frac{\omega\beta_1}{\overline{X_1}} \right] \sum_{k=1}^s \frac{b_k - ia_k}{2} \frac{z^k}{R^k} - \frac{i\overline{B}\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \sum_{k=2}^s \frac{b_k - ia_k}{2} \frac{z^{k-2}}{R^{k-2}} - \\
& \frac{\beta_1}{\overline{X_1}} \frac{(1-\Gamma)\delta_0\omega}{2\Gamma}, \quad |z| \rightarrow \infty.
\end{aligned}$$

The sum of (3.40) and (3.41) is defined by $L(z)$

$$\begin{aligned}
(3.42) \quad L(z) = & \sum_{j=1}^k j X_j z^{j-1} \sum_{k=1}^s \frac{b_k + ia_k}{2} \frac{R^k}{z^k} - 2\Omega \sum_{j=1}^k X_j z^{j-1} \sum_{k=1}^s \frac{b_k + ia_k}{2} \frac{R^k}{z^k} + \\
& \left[\Omega X_1 - \frac{\omega\beta_1}{X_1} \right] \sum_{k=1}^s \frac{b_k + ia_k}{2} \frac{R^k}{z^k} - \frac{iB\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \sum_{k=3}^s \frac{b_k + ia_k}{2} \frac{R^{k-2}}{z^{k-2}} + \\
& \overline{X_1}(\Omega - 1) - \sum_{k=1}^k j \overline{X_j} \left(\frac{R^2}{z} \right)^{j-1} \sum_{k=1}^s \frac{b_k - ia_k}{2} \frac{z^k}{R^k} - \sum_{k=1}^s (k+1) \overline{X_{k+1}} \frac{b_k - ia_k}{2} R^k + \\
& 2\Omega \left[\sum_{j=1}^k \overline{X_j} \left(\frac{R^2}{z} \right)^{j-1} \sum_{k=1}^s \frac{b_k - ia_k}{2} \frac{z^k}{R^k} + \sum_{k=1}^s \overline{X_{k+1}} \frac{b_k - ia_k}{2} R^k \right] - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0}{2} \overline{X_1} + \\
& \frac{\omega\beta_1}{\overline{X_1}} - \left[\Omega \overline{X_1} - \frac{\omega\beta_1}{\overline{X_1}} \right] \sum_{k=1}^s \frac{b_k - ia_k}{2} \frac{z^k}{R^k} - \frac{i\overline{B}\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \sum_{k=2}^s \frac{b_k - ia_k}{2} \frac{z^{k-2}}{R^{k-2}} - \\
& \frac{\beta_1}{\overline{X_1}} \frac{(1-\Gamma)\delta_0\omega}{2\Gamma},
\end{aligned}$$

such that by subtracting $L(z)$ from both the left hand side and right hand side of (3.39) we obtain the following entire function

$$\begin{aligned}
(3.43) \quad E(z) = & \begin{cases} (1 + f(z))\phi_1'(z) + \left[\frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0}{z} - \frac{2\Omega(1+f(z))}{z} \right] \phi_1(z) + \\ (1 + f(z)) \left[\Omega X_1 - \frac{iBz^2}{R^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} - \frac{\omega\beta_1}{X_1} \right] - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0}{2} X_1 + \\ \frac{\beta_1}{2X_1} \frac{(1-\Gamma)\omega\delta_0}{\Gamma} - L(z), \quad z \in D_1, \\ \\ -(1 + f(z))\overline{\phi_1}'(R^2/z) + \\ \left[\frac{2\Omega(1+f(z))z}{R^2} - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0 z}{R^2} \right] \overline{\phi_1}(R^2/z) - \\ (1 + f(z)) \left[\Omega \overline{X_1} - \frac{\omega\beta_1}{\overline{X_1}} + \frac{i\overline{B}R^2}{z^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \right] + \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0}{2} \overline{X_1} - \\ \frac{\beta_1}{2\overline{X_1}} \frac{(1-\Gamma)\delta_0\omega}{\Gamma} - L(z), \quad z \in D_2. \end{cases}
\end{aligned}$$

Once again we seek to take advantage of Louisville's theorem whereby it is realized that $E(z) = \text{constant}$ in (3.43). Owing to the subtraction of $L(z)$, $E(z) = 0$ and we generate the following two equations

$$(3.44) \quad (1 + f(z))\phi_1'(z) + \left[\frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{z} - \frac{2\Omega(1 + f(z))}{z} \right] \phi_1(z) + \\ (1 + f(z)) \left[\Omega X_1 - \frac{iBz^2}{R^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} - \frac{\omega\beta_1}{X_1} \right] - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{2} X_1 + \\ \frac{\beta_1}{2X_1} \frac{(1 - \Gamma)\omega\delta_0}{\Gamma} - L(z) = 0, \quad z \in D_1,$$

$$(3.45) \quad -(1 + f(z))\overline{\phi_1'}(R^2/z) + \\ \left[\frac{2\Omega(1 + f(z))z}{R^2} - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0 z}{\Gamma} \frac{1}{R^2} \right] \overline{\phi_1}(R^2/z) - \\ (1 + f(z)) \left[\Omega \overline{X_1} - \frac{\omega\beta_1}{\overline{X_1}} + \frac{i\overline{B}R^2}{z^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \right] + \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{2} \overline{X_1} - \\ \frac{\beta_1}{2\overline{X_1}} \frac{(1 - \Gamma)\delta_0\omega}{\Gamma} - L(z) = 0, \quad z \in D_2.$$

The compatibility requirement between (3.44) and (3.45) is given by allowing $|z| \rightarrow 0$ in (3.45)

$$(3.46) \quad L_0 = -\overline{L_0},$$

where

$$(3.47) \quad L_0 = X_1(1 - \Omega) - \frac{\omega\beta_1}{X_1} + \sum_{k=1}^s (k + 1 - 2\Omega)X_{k+1} \frac{b_k + ia_k}{2} R^k + \\ \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{2} X_1 + \frac{\beta_1(1 - \Gamma)\omega\delta_0}{2\Gamma X_1} - \frac{iB\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \frac{b_2 + ia_2}{2}.$$

Given equation (3.46), equations (3.44) and (3.45) are equivalent and hence we may use (3.44) to define a simplified differential equation for $\phi_1(z)$ as follows

$$(3.48) \quad \phi_1'(z) + \left[\frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))\delta_0}{\Gamma} \frac{1}{z(1 + f(z))} - \frac{2\Omega}{z} \right] \phi_1(z) = P(z), \quad z \in D_1,$$

where

$$(3.49) \quad P(z) = \frac{\omega\beta_1}{X_1} - \Omega X_1 + \frac{iBz^2}{R^2} \frac{\omega}{\Gamma\alpha_2 - \alpha_2 + 1} - \frac{\delta_0/2}{1 + f(z)} \left[\frac{\beta_1(1 - \Gamma)\omega}{\Gamma X_1} - \frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} X_1 \right] + \frac{L(z)}{1 + f(z)}.$$

Equation (3.48) is a first order ordinary differential equation with variable coefficients which has the following general solution

$$(3.50) \quad \phi_1(z) = e^{-T(z)} \int_{z_1}^z e^{T(z)} P(z) dz + C_0 e^{-T(z)}, \quad z \in D_1,$$

where

$$(3.51) \quad T(z) = \int \left(\frac{\omega(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} \frac{\delta_0}{z(1 + f(z))} - \frac{2\Omega}{z} \right) dz,$$

and z_1 is any point in D_1 and C_0 is an arbitrary constant of integration. In light of the fact that $P(z)$ in (3.50) contains the X_{s+1} coefficients of the power series expansion of $\phi_1(z)$, any solution of (3.50) must satisfy the consistency condition given by

$$(3.52) \quad X_k = \frac{\phi_1^k(0)}{k!}, \quad k = 1, 2, \dots, s, s+1,$$

We may derive equation (3.52) by first recalling that since $\phi_1(z)$ is analytic it has a Taylor series expansion in D_1 given by

$$(3.53) \quad \phi_1(z) = \sum_{k=0}^{\infty} Q_k z^k, \quad Q_k = \frac{\phi_1^k(0)}{k!}.$$

Then, by substituting (3.53) into (3.44) and comparing coefficients of negative powers of z as we arrive at the following

$$(3.54) \quad \sum_{j=1}^k (j - 2\Omega) Q_j z^{j-1} \sum_{k=1}^s \frac{(b_k + ia_k)}{2} \frac{R^k}{z^k} = \sum_{j=1}^k (j - 2\Omega) X_j z^{j-1} \sum_{k=1}^s \frac{(b_k + ia_k)}{2} \frac{R^k}{z^k}.$$

Careful inspection of (3.54) reveals that when $\Omega \neq 1/2$ (3.52) is true for all s . However, for the case of $\Omega = 1/2$ we see that the first statement of (3.54) will be an identity, which provides no information on the form of the coefficient X_1 and implies (3.52) is not automatically satisfied for $k = 1$. Hence we must impose the additional requirement that

$$(3.55) \quad X_1 = \phi_1'(0).$$

In general, the solution for $\phi_1(z)$ in (3.50) is not holomorphic in the uncut domain D_1 due to the presence of multivalued logarithmic functions from under the integral and from isolated singular points stemming from the zeros of the interface function $(1 + f(z))$. To ensure the holomorphicity of $\phi_1(z)$ the domain must be cut appropriately such that $\phi_1(z)$ both single valued and bounded at all isolated singular points.

4. A Specific Class of Inhomogeneous Interface

To illustrate an example we shall consider a specific form of the interface function $\delta(\theta)$ as follows

$$(4.1) \quad \delta(\theta) = \frac{\delta_0}{1 + b_s \cos(s\theta)}, \quad \delta_0 > 0, \quad -1 < b_s < 1.$$

Upon converting (4.1) into a complex variable form it is seen that there will be singularities in the interface function originating from the roots of the following polynomial of degree $2s$

$$(4.2) \quad \frac{2}{b_s} \left(\frac{z}{R} \right)^s + \left(\frac{z}{R} \right)^{2s} + 1 = 0.$$

Of the $2s$ roots of (4.2), s will lie inside D_1 and the remaining s will lie in D_2 . Let the s roots inside D_1 be denoted by

$$(4.3) \quad \rho_1, \rho_2, \rho_3, \dots, \rho_s,$$

where $\rho_{(1,2,\dots,s)}^s = \rho^*$ and ρ^* is real and given by

$$(4.4) \quad \rho^* = \begin{cases} \sqrt{\frac{1}{b_s^2} - 1} - \frac{1}{b_s}, < 0, b_s > 0, \\ -\sqrt{\frac{1}{b_s^2} - 1} - \frac{1}{b_s}, > 0, b_s < 0, \end{cases}$$

such that $-1 < \rho^* < 1$, and the remaining s roots in D_2 are given by $\frac{1}{\rho_1}, \frac{1}{\rho_2}, \dots, \frac{1}{\rho_s}$. As a consequence of the above interface definitions we make note of the following

$$(4.5) \quad \begin{aligned} -\frac{2}{b_s} &= \frac{1 + \rho^{*2}}{\rho^*}, \\ \frac{R\delta_0}{z(1+f(z))} &= -\frac{\lambda(\frac{z}{R})^{s-1}}{(\frac{z}{R})^s - \rho^*} + \frac{\lambda(\frac{z}{R})^{s-1}}{(\frac{z}{R})^s - \frac{1}{\rho^*}}, \\ \lambda &= -\delta_0 \left(\frac{1 + \rho^{*2}}{1 - \rho^{*2}} \right) < 0, \\ \frac{1}{1+f(z)} &= \frac{\frac{2}{b_s}(\frac{z}{R})^s}{[(\frac{z}{R})^s - \rho^*][(\frac{z}{R})^s - \frac{1}{\rho^*}]}. \end{aligned}$$

Utilizing (4.5) we may express (3.50) as follows

$$(4.6) \quad \begin{aligned} \phi_1(z) &= \left(\frac{z}{R}\right)^{2\Omega} \left[\left(\frac{z}{R}\right)^s - \rho^*\right]^{\frac{\lambda\Omega\eta}{s}} \left[\left(\frac{z}{R}\right)^s - \frac{1}{\rho^*}\right]^{\frac{-\lambda\Omega\eta}{s}} \int_{z_1}^z \left(\frac{t}{R}\right)^{-2\Omega+1} \left[\left(\frac{t}{R}\right)^s - \rho^*\right]^{\frac{-\lambda\Omega\eta}{s}} \\ &\quad \left[\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*}\right]^{\frac{\lambda\Omega\eta}{s}} \frac{P(t)}{\frac{t}{R}} dt, \quad z \in D_1, \\ \eta &= \frac{\Gamma\alpha_2 - \alpha_2 + 1}{\Gamma(1 - \alpha_2)} > 0, \end{aligned}$$

where the integration path is taken along the edge of any branch cuts originating from each of the s branch points. In addition, to ensure boundedness of $\phi_1(z)$ at $z = R\rho_k$ we set $C_0 = 0$ and we require that

$$(4.7) \quad \int_{R\rho_1}^{R\rho_k} \left(\frac{t}{R}\right)^{-2\Omega+1} \left[\left(\frac{t}{R}\right)^s - \rho^*\right]^{\frac{-\lambda\Omega\eta}{s}} \left[\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*}\right]^{\frac{\lambda\Omega\eta}{s}} \frac{P(t)}{\frac{t}{R}} dz = 0, \quad k = 2, 3, \dots, s,$$

in order to maintain boundedness of $\phi_1(z)$ at any of the potential isolated singular points $R\rho_k, k = 2, 3, \dots, s$ in D_1 . Additionally, by taking the difference

$$(4.8) \quad \phi_1(z^+) - \phi_1(z^-) = 0,$$

we may prove that (4.6) is continuous across any of the s branch cuts by noting that, due to the sign change of the exponents in and outside of the integral, any increments in the multivalued logarithmic terms that will arise from inside the integral will be nullified from which (4.8) is easily confirmed. The remaining irregular point to be considered is when $z = 0$. Closer inspection of (4.6) reveals that there are three cases to be considered as $z \rightarrow 0$.

4.1. Case One: $\Omega > \frac{1}{2}$.

When $\Omega > \frac{1}{2}$ we see from (4.6) that $\phi_1(z) \rightarrow 0$ as $z \rightarrow 0$. However, in order to ensure the holomorphicity of $\phi_1(z)$ we must ensure that $\phi_1(z)$ is continuous across the branch cut formed from $z = R\rho^*$ along the real axis inside D_1 . Closer inspection of (4.6) reveals the presence of an unintegrable singularity at $z = 0$. Hence we must define a new path of integration, L^* , to skirt around a neighborhood of $z = 0$ and set $z = z^*$, where z^* is any particular point on the branch cut from $z = 0$, to compensate for this change. In this way the continuity condition becomes

$$(4.9) \quad \int_{L^*} \left(\frac{z^*}{t}\right)^{-2\Omega} \left[\frac{\left(\frac{z^*}{R}\right)^s - \rho^*}{\left(\frac{t}{R}\right)^s - \rho^*} \right]^{\frac{-\lambda\Omega\eta}{s}} \left[\frac{\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*}}{\left(\frac{z^*}{R}\right)^s - \frac{1}{\rho^*}} \right]^{\frac{\lambda\Omega\eta}{s}} P(t) dt = 0$$

We may then solve for the X_{s+1} unknown coefficients using (3.32,3.46,4.10) and in cases of $s > 1$, (4.7).

4.2. Case Two: $\Omega < \frac{1}{2}$.

For this case we shall rewrite (4.6) in the form

$$(4.10) \quad \frac{\phi_1(z)}{\frac{z}{R}} = \left(\frac{z}{R}\right)^{2\Omega-1} \left[\left(\frac{z}{R}\right)^s - \rho^* \right]^{\frac{\lambda\Omega\eta}{s}} \left[\left(\frac{z}{R}\right)^s - \frac{1}{\rho^*} \right]^{\frac{-\lambda\Omega\eta}{s}} \int_{R\rho_1}^z \left(\frac{t}{R}\right)^{-2\Omega} \left[\left(\frac{t}{R}\right)^s - \rho^* \right]^{\frac{-\lambda\Omega\eta}{s}} \left[\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*} \right]^{\frac{\lambda\Omega\eta}{s}} P(t) dt, \quad z \in D_1.$$

Given that $X_0 = 0$, the LHS of (4.10) is analytic within D_1 . As a consequence, $\frac{\phi_1(z)}{\frac{z}{R}}$ must be bounded at $z = 0$ and since $\Omega < \frac{1}{2}$ this implies that

$$(4.11) \quad \int_{R\rho_1}^0 \left(\frac{t}{R}\right)^{-2\Omega} \left[\left(\frac{t}{R}\right)^s - \rho^* \right]^{\frac{-\lambda\Omega\eta}{s}} \left[\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*} \right]^{\frac{\lambda\Omega\eta}{s}} P(t) dt = 0, \quad \Omega < \frac{1}{2}.$$

Note that in (4.11) there is a singularity in the integrand owing to the term $\left(\frac{t}{R}\right)^{-2\Omega}$ for $\Omega < \frac{1}{2}$. Due to the fact that the path of integration in (4.11) lies on the real axis we may treat

$$(4.12) \quad K(\rho^*, t) = \left(\frac{t}{R}\right)^{-2\Omega} \left[\left(\frac{t}{R}\right)^s - \rho^* \right]^{\frac{-\lambda\Omega\eta}{s}} \left[\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*} \right]^{\frac{\lambda\Omega\eta}{s}},$$

as a proper singular kernel function on such that (4.11) belongs to a class of Hölder continuous functions of ρ^* and is thusly integrable along such a domain [?]. We may then solve for the X_{s+1} unknown coefficients using (3.32,3.46,4.11) and in cases of $s > 1$, (4.7).

4.3. Case Three: $\Omega = \frac{1}{2}$.

In this case from (4.6) we see that $z = 0$ is not a singular point of $\phi_1(z)$ and hence $\phi_1(0) = 0$. We may then proceed to solve for the X_{s+1} unknown coefficients by recalling relation (3.46) and by evaluating (3.52) as

$$(4.13) \quad RX_1 = [-\rho^*]^{\frac{\lambda\eta}{2s}} \left[-\frac{1}{\rho^*} \right]^{\frac{-\lambda\eta}{2s}} \int_{R\rho_1}^0 \left[\left(\frac{t}{R}\right)^s - \rho^* \right]^{\frac{-\lambda\eta}{2s}} \left[\left(\frac{t}{R}\right)^s - \frac{1}{\rho^*} \right]^{\frac{\lambda\eta}{2s}} \frac{P(t)}{\frac{t}{R}} dt = 0.$$

The $s + 1$ unknown coefficients are then determined from (3.32,3.46,4.13) and in cases of $s > 1$, (4.7).

5. Example

For ease of analysis in illustrating the method we shall assume that $\Omega = \frac{1}{2}$, $\lambda = -1$, $\eta = 2$ and we shall confine ourselves to the case $s = 1$. From these preliminaries we may evaluate (4.6) as

$$(5.1) \quad \phi_1(z) = \frac{z}{R} \left(\frac{z/R - 1/\rho^*}{z/R - \rho^*} \right) \left[I_1(z) \left(\omega\beta_1 \left(\frac{1}{X_1} + \frac{1}{\overline{X_1}} \right) - \frac{1}{2} (X_1 + \overline{X_1}) \right) + \right. \\ \left. X_2 R I_2(z) + \delta_0 (2/b_1) \frac{\omega\beta_1(\alpha_1 - \Gamma(\alpha_1 - 1))}{\Gamma} X_1 I_2(z) + \frac{iB\omega}{\Gamma\alpha_2 - \alpha_2 + 1} I_3(z) \right], \quad z \in D_1,$$

where

$$(5.2) \quad I_1(z) = \int_{R\rho^*}^z \frac{t/R}{(t/R - 1/\rho^*)^2} dt, \\ I_2(z) = \int_{R\rho^*}^z \frac{1}{(t/R - 1/\rho^*)^2} dt, \\ I_3(z) = \int_{R\rho^*}^z \frac{t/R(t/R - \rho^*)}{(t/R - 1/\rho^*)^2} dt, \quad z \in D_1.$$

The unknown coefficients $X_1, \overline{X_1}, X_2, \overline{X_2}$ are then evaluated from (3.46, 4.13) as follows

$$(5.3) \quad \frac{1}{2} (X_1 + \overline{X_1}) - \omega\beta_1 \left(\frac{1}{X_1} + \frac{1}{\overline{X_1}} \right) + \frac{b_1}{2} R (X_2 + \overline{X_2}) = \\ \frac{\delta_0}{2} \left[\frac{\omega(\Gamma(\alpha_1 - 1) - \alpha_1)}{\Gamma} (X_1 + \overline{X_1}) + \frac{\beta_1(\Gamma - 1)\omega}{\Gamma} \left(\frac{1}{X_1} + \frac{1}{\overline{X_1}} \right) \right],$$

$$(5.4) \quad \left[\frac{R\rho^{*2}}{\rho^{*2} - 1} + R \ln \left(\frac{1}{1 - \rho^{*2}} \right) \right] \left(\omega\beta_1 \left(\frac{1}{X_1} + \frac{1}{\overline{X_1}} \right) - \frac{1}{2} (X_1 + \overline{X_1}) \right) \\ + X_2 R \left(\frac{R\rho^{*3}}{\rho^{*2} - 1} \right) + \frac{iB\omega}{\Gamma\alpha_2 - \alpha_2 + 1} \left[\frac{R(1 - \rho^{*2})}{\rho^{*2}} \ln \left(\frac{1}{1 - \rho^{*2}} \right) + \frac{R\rho^{*2}}{2} - R \right] = 0, \\ -1 < \rho_1 < 1.$$

Noting that $\frac{1}{2} = 1 - \Omega$ it can be shown that since $\frac{\delta_0}{2} = \frac{nR}{2\mu_2}$, (5.3) is in fact identical to (3.22) in the case where $\rho_1 \rightarrow 0$.

6. Results

Having verified the formulation we may now proceed to compare the homogeneous imperfect interface to the inhomogeneous one. For the purpose of this example we will compare the inhomogeneous interface of the form

$$(6.1) \quad \frac{n(\theta)R}{\mu_2} = \frac{\delta_0}{1 + b_1 \cos(\theta)}, \quad \delta_0 = \frac{1 - \rho_1^2}{1 + \rho_1^2}, \quad -1 < b_1 < 1,$$

to the homogeneous imperfect interface given by

$$(6.2) \quad \frac{nR}{\mu_2} = \delta_0.$$

Close inspection of the expression given by (3.4) reveals that in the cases of either a uniaxial or biaxial remote loading, B is in fact purely real. Hence we may prove from (5.3,5.4) that X_1, X_2 must both be purely imaginary and we may solve for them using (3.46,5.3,5.4). Computing the average mean stress on the boundary defined by

$$(6.3) \quad (P_{11} + P_{22})_{2,Avg} = \frac{1}{C_{\partial D_1}} \int_{\partial D_1} 4\mu_2 \text{Im} \left[\Gamma(1 - \alpha_1)X_1 + \frac{\Gamma\beta_1}{X_1} \right] ds,$$

the ratio of the inhomogeneous to homogeneous interfaces will be one to one since X_1 is identical in both interface conditions. In an attempt to explore further the results we compute the ratio of the mean stresses at $z = R$ given by the relations

$$(6.4) \quad (P_{11} + P_{22})_{2,Homogeneous} = 4\mu_2 \text{Im} \left[\Gamma(1 - \alpha_1)(X_1) + \frac{\Gamma\beta_1}{X_1} \right],$$

$$(6.5) \quad (P_{11} + P_{22})_{2,Inhomogeneous} = 4\mu_2 \text{Im} \left[\Gamma(1 - \alpha_1)(X_1 + 2X_2z) + \frac{\Gamma\beta_1}{X_1 + 2X_2z} \right],$$

from which the following results are observed

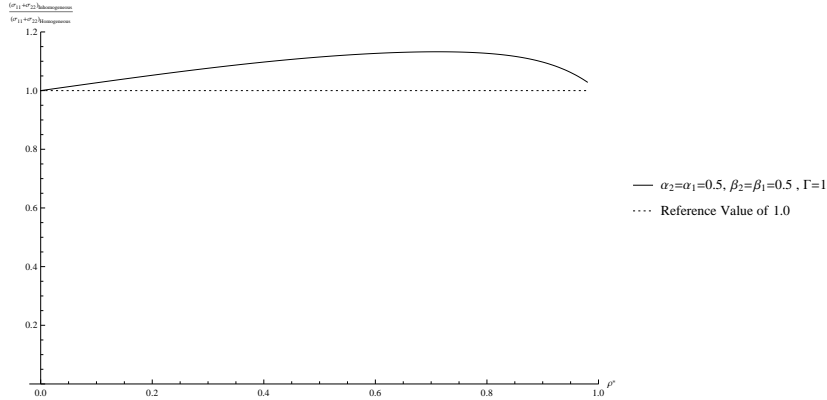


FIGURE 2. Ratio of inhomogeneous to homogeneous mean stress at $z = R$ for the remote loading $P_{11}^\infty = 0, P_{22}^\infty = 1, P_{12}^\infty = 0$

From Figure 2 we conclude that the inhomogeneous interface parameter ρ^* does have an influence on the mean stress at the point $z = R$ on the boundary ∂D_1 , which at its peak reaches an error of 13 percent. In contrast, Ru [25] observed a relative error in the mean stress of up to 80 percent in the case of a inhomogeneous sliding interface in linear elasticity. While the present work does not reach relative errors of a similar magnitude we cannot simply ignore the effects of the circumferential variation of the interface in the finite deformation setting. Therefore, replacing the circumferential variation of the interface by its homogenous counterpart will contribute to a modest relative error.

7. Conclusions

The general solution for the case of an inhomogeneous imperfect sliding interface characterized by the imperfect interface parameters $m(\theta) \rightarrow \infty, n(\theta) = \text{finite}$ is presented. The formulation has been validated by referring to the solution of a homogeneous imperfect interface under the same sliding interface boundary conditions and subsequently results were presented for the mean stress at a specific point along the inclusion matrix boundary curve under remote loads. From these results it was observed

that the average mean stress within the inclusion was identical between the inhomogeneous and homogeneous interface conditions and that there was a maximum error of 13 percent when comparing the mean stress at a point on the interface between the inhomogeneous and homogeneous models. Thus, replacing the circumferential variation of the interface by its homogenous counterpart will contribute to a modest relative error in not only the mean stress but the field quantities as well.

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References

- [1] J. Eshelby, The Determination of the Elastic Field of an Ellipsoidal Inclusion, and Related Problems, *Proceedings of the Royal Society. A, Mathematical, Physical and Engineering Sciences*, **241**, 1226, 376-396, 1957.
- [2] N.I. Muskhelishvili, *Some Basic Problems of the Mathematical Theory of Elasticity*, P. Noordhoff, Groningen, The Netherlands, 1953.
- [3] C.Q. Ru, Analytic solution for Eshelby's problem of an inclusion of arbitrary shape in a plane or half-plane, *Journal of Applied Mechanics*, **68**, 315-322, 1999.
- [4] C.Q. Ru, P. Schiavone, A. Mioduchowski, Elastic fields in two jointed half-planes with an inclusion of arbitrary shape, *Z. angew. Math. Phys.*, **52**, 18-32, 2001.
- [5] X. Wang, L.J. Sudak, Interaction of screw dislocation with an arbitrary shaped elastic inhomogeneity, *Journal of Applied Mechanics*, **73**, 206-211, 2006.
- [6] Z. Hashin, The spherical inclusion with imperfect interface, *Journal of Applied Mechanics*, **58**, 444-449, 1991.
- [7] Z. Gao, A circular inclusion with imperfect interface: Eshelby's tensor and related problems, *Journal of Applied Mechanics*, **62**, 860-866, 1995.
- [8] L.J. Sudak, X. Wang, An irregular-shaped inclusion with imperfect interface in antiplane elasticity, *Acta Mechanica*, **224**, 9, 2009-2023, 2013.
- [9] S. Lurie, P. Belov, D. Volkov-Bogorodsky, N. Tuchkova, Interphase layer theory and applications in the mechanics of composite materials, *J. Mater. Sci.*, **41**, 20, 6693-6707, 2006.
- [10] F. John, Plane strain problems for a perfectly elastic material of harmonic type, *Communications on Pure and Applied Mathematics*, **13**, 239-296, 1960.
- [11] R.W. Ogden, D.A. Isherwood, Solutions of some finite plane-strain problems for compressible elastic solids, *Quarterly Journal of Mechanics and Applied Mathematics*, **XXXI**, 3, 219-249, 1977.
- [12] E. Varley, E. Cumberbatch, Finite deformations of elastic materials surrounding cylindrical holes, *Journal of Elasticity*, **10**, 4, 341-405, 1980.
- [13] E. Knowles, J.K. Sternberg, On the singularity induced by certain mixed boundary conditions in linearized and nonlinear elastostatics, *International Journal of Solids and Structures*, **11**, 11, 1173-1201, 1975
- [14] C.Q. Ru, On complex-variable formulations for finite plane elastostatics of harmonic materials, *Acta Mechanica*, **234**, 156, 219-234, 2002.
- [15] C.Q. Ru, P. Schiavone, L.J. Sudak, A. Mioduchowski, Uniformity of stresses inside and elliptic inclusion in finite plane elastostatics, *International Journal of Non-Linear Mechanics*, **40**, 281-287, 2005.
- [16] C.I. Kim, P. Schiavone, Designing an inhomogeneity with uniform interior stress in finite plane elastostatics, *Acta Mechanica*, **197**, 285-299, 2008.
- [17] X. Wang, E. Pan, On partially debonded circular inclusion in finite plane elastostatics of harmonic materials, *Journal of Applied Mechanics*, **76**, 1-5, 2008.
- [18] X. Wang, A circular inclusion with imperfect interface in finite plane elastostatics, *Acta Mechanica*, **491**, 481-491, 2012.
- [19] D.R. McArthur, L.J. Sudak, A circular inclusion with circumferentially inhomogeneous imperfect interface in harmonic materials, *Continuum Mechanics and Thermodynamics*, **28**, 317-329, 2016.

- [20] D.R. McArthur, L.J. Sudak, A circular inclusion with inhomogeneous non-slip imperfect interface in harmonic materials, *Proceedings of the Royal Society. A, Mathematical, Physical and Engineering Sciences*, **472**, 2190, 2016.
- [21] S. Mijailovich, D. Stamenovic, J. Fredberg, Toward a kinetic theory of connective tissue micromechanics, *Journal of Applied Physiology*, **74**, 2, 665-681, 1993.
- [22] H. Van Swygenhoven, Plastic deformation in metals with nanosized grains: Atomistic simulations and experiments, *Materials Science Forum*, **447-448**, 3-10, 2004.
- [23] L. Wei, Y.J. Anand, Grain-boundary sliding and separation in polycrystalline metals: applications to nanocrystalline fcc metals, *Journal of the Mechanics and Physics of Solids*, **52**, 2587-2616, 2004.
- [24] D. Barton, P. Drikakis, An Eulerian method for multi-component problems in non-linear elasticity with sliding interfaces, *Journal of Computational Physics*, **229**, 5518-5540, 2010.
- [25] C.Q. Ru, A circular inclusion with circumferentially inhomogeneous sliding interface in plane elastostatics, *Journal of Applied Mechanics*, **65**, 1, 30-38, 1998.

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